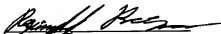


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METHOD AND APPARATUS FOR FAST DTMF DETECTION

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METHOD AND APPARATUS FOR FAST DTMF DETECTION

FIELD OF THE INVENTION

[0001] This invention relates to signal processing in packet-based networks and, in particular, to DTMF detection.

BACKGROUND OF THE INVENTION

[0002] Dual tone multi-frequency (DTMF) signals were originally developed to facilitate the automated dialing of telephone numbers by end-users. They have since found wider application in transmitting other information, such as for example in voice mail systems and automated telephone menu systems. In the public switched telephone network (PSTN), DTMF signals are transmitted in-band with voice signals. A set of standards have been developed to set specifications for how DTMF is to be generated and when a DTMF tone should be recognized. For example the International Telecommunications Union has developed standards ITU-T Q.23 and ITU-T Q.24.

[0003] A DTMF signal is a sum of two predetermined frequencies, one selected from a set of four low frequency tones, and one selected from a set of four high frequency tones. Each pair of tones represents one of sixteen keys. The standard telephone keypad only uses the first twelve keys, and not the four alphanumeric keys (A to D), which are reserved for future use. The frequencies and their corresponding keys are outlined below in Table 1.

TABLE 1

$f(\text{Hz})$	1209	1336	1477	1633
697	1	2	3	A
770	4	5	6	B
852	7	8	9	C
941	*	0	#	D

[0004] Digital packet-based networks, like the Internet, are increasingly being used for transmission of telephone signals. The use of packet-based networks for telephony presents a problem for DTMF signaling. The compression techniques used for preserving bandwidth in packet-based networks are acceptable for speech, since the associated degradation is tolerable; however, these compression techniques degrade DTMF signals to an extent that they no longer satisfy the standards and will fail to be recognized at the receiver.

[0005] In order to address this problem, packet-based networks may attempt to detect DTMF tones in a voice signal so as to strip them out before transmitting the voice signal. The DTMF tones represent alphanumeric information, and can easily and more efficiently be sent as a separate binary signal, or be otherwise encoded in the packetized linear voice signal. Accordingly, a packet-based network may employ a DTMF detector.

[0006] Another difficulty encountered with packet-based signals is that of end-to-end delay. Delay results from the processing associated with packetization and compression, and from the inherent delay in transmission through routers. Delay in packet-based telephony is particularly noticeable to the users.

[0007] Detecting a DTMF tone takes a certain amount of time, and the lag associated with this detection time can

result in a portion of the DTMF tone leaking in-band prior to the detection occurring and prior to triggering a muting of the DTMF tone. At the receiving end, this leaked portion will be recombined with a regenerated DTMF signal and can result in spectral line splitting, which in turn can result in a failure to detect a valid DTMF digit. In some cases, it can lead to the false detection of double digits.

[0008] To avoid the spectral line splitting problem, a transmission delay must be incorporated so as to hold the voice packet while the DTMF detector attempts to detect a DTMF signal. The voice packet is only sent once the DTMF detector has finished analyzing whether or not the packet contains a DTMF signal. Therefore, DTMF detectors having a significant delay will further aggravate the delay problems of packet-based telephony.

[0009] Existing DTMF detectors typically require at least 10 milliseconds to analyze a packet for DTMF signals.

[0010] Accordingly, there remains a need for a DTMF detector that is capable of detecting DTMF signals quickly.

SUMMARY OF THE INVENTION

[0011] The present invention provides a DTMF detector that filters an incoming packetized linear voice signal through a set of parallel notch filters to knock down the potential DTMF tones. Each notch filter includes two notches corresponding to a selected pair of DTMF frequencies making up a DTMF tone. The energy levels of the resulting filtered signals are analyzed and this information is used to assess whether the incoming signal

contains a DTMF tone.

[0012] In one aspect, the present invention provides a method for detecting DTMF signals in a packetized linear voice signal. The method includes the steps of filtering the packetized linear voice signal through a plurality of notch filters, each of the notch filters having a pair of notches at DTMF frequencies and each of the notch filters producing a filtered signal, calculating an energy level for each of the filtered signals, evaluating one or more criteria using the calculated energy levels, and, if the criteria are met, producing a DTMF indicator.

[0013] In a further aspect, the present invention provides a DTMF detector for detecting DTMF signals in a packetized linear voice signal. The DTMF detector includes a plurality of notch filters each having a pair of notches at DTMF frequencies and each of the notch filters receiving the packetized linear voice signal and producing a filtered signal, a calculating module for calculating an energy level for each of the filtered signals, and an evaluating module for evaluating one or more criteria using the energy levels and, if the criteria are met, producing a DTMF indicator.

[0014] Other aspects and features of the present invention will become apparent to those ordinarily skilled in the art upon review of the following description of specific embodiments of the invention in conjunction with the accompanying figures.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] Reference will now be made, by way of example, to the accompanying drawings which show an embodiment of the present invention, and in which:

[0016] Figure 1 shows a block diagram of an embodiment of a DTMF detector according to the present invention; and

[0017] Figure 2 shows, in flowchart form, a method of detecting a DTMF signal, according to the present invention.

[0018] Similar reference numerals are used in different figures to denote similar components.

DESCRIPTION OF SPECIFIC EMBODIMENTS

[0019] The following detailed description of specific embodiments of the present invention does not limit the implementation of the invention to any particular programming language or signal processing architecture. In one embodiment, the present invention is implemented, at least partly, using a digital signal processor. It will be understood that the present invention may be implemented using other architectures, including a microcontroller, a microprocessor, programmable logic arrays, discrete components, or combinations thereof. Any limitations presented herein as a result of a particular type of signal processing architecture or programming language are not intended as limitations of the present invention.

[0020] Reference is first made to Figure 1, which shows a block diagram of an embodiment of a DTMF detector 10 according to the present invention. The detector 10 includes a plurality, e.g. a set or bank, of notch filters 12. Each notch filter 12 has a transfer characteristic that features two notches corresponding to two of the DTMF frequencies. In other words, each notch filter 12 is designed to knock down the two frequencies

that make up a particular DTMF tone. In one embodiment, the notch filters 12 comprise sixteen individual notch filters 12a, 12b,..., 12p, corresponding to the sixteen DTMF tones. In such an embodiment, the notch filters 12 will each have a pair of notches roughly centered as follows:

Table 2

Filter No.	DTMF Key	Low Freq.	High Freq.
1	1	697 Hz	1209 Hz
2	2	697 Hz	1336 Hz
3	3	697 Hz	1477 Hz
4	A	697 Hz	1633 Hz
5	4	770 Hz	1209 Hz
6	5	770 Hz	1336 Hz
7	6	770 Hz	1477 Hz
8	B	770 Hz	1633 Hz
9	7	852 Hz	1209 Hz
10	8	852 Hz	1336 Hz
11	9	852 Hz	1477 Hz
12	C	852 Hz	1633 Hz
13	*	941 Hz	1209 Hz
14	0	941 Hz	1336 Hz
15	#	941 Hz	1477 Hz
16	D	941 Hz	1633 Hz

[0021] Each of the notch filters 12 receives a packetized linear voice signal 22 as an input. In one embodiment, the packetized linear voice signal 22 is arranged in frames of 5 millisecond duration, each frame containing forty samples of an input signal sampled at 8 kHz. The notch filters 12 operate upon the packetized linear voice signal 22 in parallel and output a corresponding set of notch filtered signals 24a, 24b,..., 24p.

[0022] The detector 10 further includes a signal

energy calculation module 14 coupled to the notch filters 12, arranged in parallel as shown in Figure 1, for calculating the energies of the notch filtered signals 24. The signal energy calculation module 14 generates signal energy information 30.

[0023] The signal energy information 30 is provided to a threshold criteria evaluation module 16. The threshold criteria evaluation module 16 applies several criteria to the signal energy information 30 to determine whether or not the packetized linear voice signal 22 contains a DTMF tone. Based upon this evaluation, the threshold criteria evaluation module 16 generates a DTMF indicator 32 that signals if a DTMF tone is present.

[0024] In one embodiment, the detector 10 further includes additional notch filters for applying additional criteria at the evaluation stage. For example, the detector 10 includes a 1004 Hz filter 18 to knock down a tone at 1004 Hz that can occasionally cause false DTMF tone detection. In addition, the detector 10 includes a dial tone filter 20 for knocking down the dial tone, which results from the combination of the dial tone frequencies 350 Hz and 440 Hz. In one embodiment, the dial tone filter 20 is a notch filter at 400 Hz.

[0025] The 1004 Hz filter 18 produces a 1004 Hz filtered signal 26, and the dial tone filter 20 produces a dial tone filtered signal 28, both of which are input to the signal energy calculation module 14. The packetized linear voice signal 22 may also be input to the signal energy calculation module 14.

[0026] The coefficients for establishing the notch filters 12 may be obtained offline through an adaptive algorithm. For example, the notch filters 12 may be designed as 4th order FIR filters using Burg's method.

Once the appropriate coefficients are obtained through an offline adaptive algorithm, they are used to establish the notch filters 12.

[0027] Reference is now made to Figure 2, which shows, in flowchart form, a method 100 of detecting DTMF signals in the packetized linear voice signal 22 (Fig. 1).

[0028] The method 100 begins in step 102 where the packetized linear voice signal 22 is filtered through the notch filters 12 (Fig. 1). The resulting filtered signals 24 (Fig. 1) are input to the signal energy calculation module 14 (Fig. 1). In step 104, the signal energy calculation module 14 calculates the signal energies of the filtered signals 24. The signal energy calculation module 14 may also calculate the signal energies of the 1004 Hz filtered signal 26 (Fig. 1), the dial tone filtered signal 28 (Fig. 1), and the input packetized linear voice signal 22 (Fig. 1).

[0029] In one embodiment, the notch filtered signal 24 output by the notch filters 12 are obtained through the difference equation:

$$y_x(k) = a_{x0}r(k) + a_{x1}r(k-1) + a_{x2}r(k-2) \\ + a_{x3}r(k-3) + a_{x4}r(k-4)$$

where $r(k)$ is the packetized linear voice signal 22 sample at instant k , and the coefficients a_{xi} of the notch filters 12 are obtained offline by Burg's algorithm. The table below details the calculated coefficients a_{xi} for one embodiment:

Table 3					
Filter x	Coefficient				
	a_{x0}	a_{x1}	a_{x2}	a_{x3}	a_{x4}
1	0.100000	-0.287197	0.398812	-0.287197	0.099999

2	0.100000	-0.270422	0.370163	-0.270422	0.099999
3	0.100000	-0.250646	0.336387	-0.250646	0.099999
4	0.100000	-0.227636	0.297089	-0.227636	0.099999
5	0.100000	-0.280953	0.391545	-0.280953	0.099999
6	0.100000	-0.264179	0.363944	-0.264179	0.099999
7	0.100000	-0.244403	0.331403	-0.244403	0.099999
8	0.100000	-0.221393	0.293541	-0.221393	0.099999
9	0.100000	-0.273296	0.382631	-0.273296	0.099999
10	0.100000	-0.256522	0.356315	-0.256522	0.099999
11	0.100000	-0.236746	0.325289	-0.236746	0.099999
12	0.100000	-0.213736	0.289189	-0.213736	0.099999
13	0.100000	-0.264249	0.372100	-0.264249	0.099999
14	0.100000	-0.247475	0.347302	-0.247475	0.099999
15	0.100000	-0.227699	0.318065	-0.227699	0.099999
16	0.100000	-0.204689	0.284047	-0.204689	0.099999

[0030] The dial tone filtered signal 28 is obtained using the difference equation:

$$Z(k) = b_0 r(k) + b_1 r(k-1) + b_2 r(k-2)$$

where b_0 , b_1 , b_2 are the dial tone filter coefficients, which in one embodiment are calculated to be:

$$b_0=1;$$

$$b_1=-1.999997; \text{ and}$$

$$b_2=1.$$

[0031] Similarly, the 1004Hz filtered signal 26 is obtained from the difference equation:

$$g(k) = d_0 r(k) + d_1 r(k-1) + d_2 r(k-2)$$

where d_0 , d_1 , d_2 are the 1004Hz filter coefficients, which in one embodiment are calculated to be:

$$d_0=1;$$

$d_1 = -1.9998$; and

$d_2 = 1$.

[0032] The calculation of signal energy by the signal energy calculation module 14 is performed on a frame-by-frame basis for each signal normalized to the frame energy of the packetized linear voice signal 22. If a frame for the input packetized linear voice signal 22 includes 40 samples $r(n)$, where $n = 1$ to 40, then the output notch filtered signal 24 is $y(n)$. In one embodiment the signal energy of notch filtered signal $24x(x = a, b, c, \dots, p)$ is determined as:

$$NE = y^2(\mu+1) + y^2(\mu+2) + \dots + y^2(N) / \\ [r^2(\mu+1) + r^2(\mu+2) + \dots + r^2(N)]$$

where NE is the energy of notch filtered signal $24x$, μ is the order of the filter, which in one embodiment is 4, and N is the number of samples in the frame, which in one embodiment is 40. Note that in the sixth criterion, described below, the absolute energy is used since the criterion relates to the packetized linear voice signal 22 itself. The first μ samples of the filter output are not used to avoid the transient filter response.

[0033] The signal energy information 30 (Fig. 1) generated by the signal energy calculation module 14 is used by the threshold criteria evaluation module 16 (Fig. 1) to determine if a DTMF tone is present in the packetized linear voice signal 22 in step 106. The threshold criteria evaluation module 16 applies several criteria to assess whether the energies calculated for the signals from the various filters 12, 18, and 20 demonstrate the presence of a DTMF tone. In one embodiment, if all the criteria are met, then a DTMF tone is deemed to be present.

[0034] In one embodiment, the criteria include eight thresholds that must be met to signify a DTMF tone.

[0035] The first criterion is a first energy differential test. The first energy differential test evaluates whether the notch filtered signal 24 having the minimum energy level has an energy level a predetermined amount lower than the energy level of the notch filtered signal 24 having the maximum energy level. If so, then the threshold is met and indicates a possible DTMF tone.

[0036] The test is based upon the understanding that a tone at the notch frequencies for a particular notch filter 12 would result in a notch filtered signal 24 from that notch filter 12 having an energy level significantly lower than the energy levels of the notch filtered signals 24 from the other notch filters 12. The first energy differential test may be expressed as:

$$K1 * \max(\text{NE}(x)) - \min(\text{NE}(x)) \geq C1$$

where $\max(\text{NE}(x))$ is the maximum energy level among the notch filtered signals 24 for frame x , $\min(\text{NE}(x))$ is the minimum energy level among the notch filtered signals 24 for frame x , $K1$ is an empirical parameter, and $C1$ is the first criterion's threshold. In one embodiment, $K1$ is determined to be $10^{-39/20}$, and $C1$ is -0.079713 .

[0037] The second criterion is a second energy differential test. The second energy differential test assesses whether the signal energy is strongly located on one DTMF tone by assessing whether the notch filtered signal 24 having the minimum energy level has an energy level a predetermined amount lower than the notch filtered signal 24 having second lowest energy level. If the signal with the minimum level has an energy level a significant amount lower than the second-to-minimum signal, then it is indicative of a potential DTMF tone.

[0038] The second test may be expressed as:

$$K2 * \text{secmin}(\text{NE}(x)) - \min(\text{NE}(x)) \geq C2$$

where $\text{secmin}(\text{NE}(x))$ is the second-to-minimum energy level among the notch filtered signals 24 for frame x , $K2$ is an empirical parameter, and $C2$ is the second criterion's threshold. In one embodiment, $K2$ is determined to be $10^{-4/20}$ and $C2$ is -0.039857 .

[0039] The third criterion is a twist test, which is an evaluation of the twist of the two frequency components that make up the DTMF tone. For the notch filtered signal 24 having the minimum signal energy level, a comparison is made between the energy level contributions attributable to the low frequency tone and the high frequency tone. This is accomplished by analyzing two different notch filtered signals 24, each having a notch at one of either the low frequency tone or the high frequency tone of the minimum signal. For example, if the minimum signal energy level is sensed at a filter having notches at low frequency 1 and high frequency 2, then the twist test compares the signal energies produced by a filter having notches at low frequency 1 and high frequency 4 and a filter having notches at low frequency 3 and high frequency 2. The test may determine if the relative contributions of the two tones to the minimum signal energy are within an expected range.

[0040] In one embodiment, the twist test may be expressed as:

$$\begin{aligned} &(\text{NE}(\text{n+offsetLow1}(\text{n})) + \epsilon) - \\ &\text{Ktwist}(\text{n}) * (\text{NE}(\text{n+offsetHigh1}(\text{n})) + \epsilon) \geq C3 \end{aligned}$$

where $\text{NE}()$ is the signal energy, n is the filter number, $\text{offsetLow1}(\text{n})$ is an offset for filter n to isolate the

low frequency component, $\text{offsetHigh1}(n)$ is an offset for filter n to isolate the high frequency component, and K_{twist} and ϵ are empirically determined constants. In one embodiment ϵ is 10^{-15} . The table below provides the constants for $K_{\text{twist}}(n)$ according to one embodiment of the present invention. $C3$ is also an empirically determined constant, which in one embodiment is -0.01 .

Table 4	
Filter No.	Ktwist
1	0.693208
2	0.949722
3	0.692794
4	0.949279
5	0.479940
6	0.657535
7	0.479740
8	0.657311
9	0.689847
10	0.945359
11	0.689571
12	0.944877
13	0.478261
14	0.655051
15	0.477858
16	0.654666

[0041] The offsets, $\text{offsetLow1}(n)$ and $\text{offsetHigh1}(n)$ are vectors, which in one embodiment have the following values:

$\text{offsetLow1}(n) = [2 \ 2 \ -2 \ -2 \ 2 \ 2 \ -2 \ -2 \ 2 \ 2 \ -2 \ -2 \ 2 \ 2 \ -2 \ -2];$

$\text{offsetHigh1}(n) = [8 \ 8 \ 8 \ 8 \ 8 \ 8 \ 8 \ 8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8];$

[0042] Applying the above offset vectors to the twist test equation results in the following expressions of the twist test, based upon the filter number:

TABLE 5

Filter	Criteria
1	$(NE(3) + \epsilon) - K_{\text{twist}}(1) * (NE(9) + \epsilon) \geq C3$
2	$(NE(4) + \epsilon) - K_{\text{twist}}(2) * (NE(10) + \epsilon) \geq C3$
3	$(NE(1) + \epsilon) - K_{\text{twist}}(3) * (NE(11) + \epsilon) \geq C3$
4	$(NE(2) + \epsilon) - K_{\text{twist}}(4) * (NE(12) + \epsilon) \geq C3$

$$\begin{array}{ll}
5 & | \text{ (NE(7) + } \varepsilon \text{) - Ktwist(5) * (NE(13) + } \varepsilon \text{) } \geq \text{C3} \\
6 & | \text{ (NE(8) + } \varepsilon \text{) - Ktwist(6) * (NE(14) + } \varepsilon \text{) } \geq \text{C3} \\
7 & | \text{ (NE(5) + } \varepsilon \text{) - Ktwist(7) * (NE(15) + } \varepsilon \text{) } \geq \text{C3} \\
8 & | \text{ (NE(6) + } \varepsilon \text{) - Ktwist(8) * (NE(16) + } \varepsilon \text{) } \geq \text{C3} \\
9 & | \text{ (NE(11) + } \varepsilon \text{) - Ktwist(9) * (NE(1) + } \varepsilon \text{) } \geq \text{C3} \\
10 & | \text{ (NE(12) + } \varepsilon \text{) - Ktwist(10) * (NE(2) + } \varepsilon \text{) } \geq \text{C3} \\
11 & | \text{ (NE(9) + } \varepsilon \text{) - Ktwist(11) * (NE(3) + } \varepsilon \text{) } \geq \text{C3} \\
12 & | \text{ (NE(10) + } \varepsilon \text{) - Ktwist(12) * (NE(4) + } \varepsilon \text{) } \geq \text{C3} \\
13 & | \text{ (NE(15) + } \varepsilon \text{) - Ktwist(13) * (NE(5) + } \varepsilon \text{) } \geq \text{C3} \\
14 & | \text{ (NE(16) + } \varepsilon \text{) - Ktwist(14) * (NE(6) + } \varepsilon \text{) } \geq \text{C3} \\
15 & | \text{ (NE(13) + } \varepsilon \text{) - Ktwist(15) * (NE(7) + } \varepsilon \text{) } \geq \text{C3} \\
16 & | \text{ (NE(14) + } \varepsilon \text{) - Ktwist(16) * (NE(8) + } \varepsilon \text{) } \geq \text{C3}
\end{array}$$

[0043] The fourth criterion is a low frequency tolerance test. The low frequency tolerance test assesses whether the low frequency component of a suspected DTMF tone falls within the accepted tolerances. According to ITU recommendations, the low frequency signal must be within 1.5% of the target low frequency to qualify as a detected signal. One method of assessing the extent to which the low frequency signal meets this criteria is through assessing the extent to which that component of the signal is removed by the notch filter. A method of making that assessment is to compare the relative signal energies of other notch filters that include a notch at the low frequency.

[0044] In one embodiment, the low frequency tolerance test may be expressed as:

$$\text{Klf}(n) * \text{NE}(n + \text{offsetLow1}(n)) - \text{NE}(n + \text{offsetLow2}(n)) \geq \text{C4}$$

where NE() is the signal energy, n is the filter number of the filter having the minimum signal energy, offsetLow1(n) is an offset for filter n to select a filter having a notch at the low frequency component, offsetLow2(n) is an offset for filter n to select another filter having a notch at the low frequency component, and

Klf and C4 are empirically determined constants. In one embodiment, C4 is -0.057 and Klf(n) has the values shown in the table below:

Table 6	
Filter No.	Klf
1	0.344174
2	0.344174
3	0.344174
4	0.344174
5	0.352217
6	0.352217
7	0.352217
8	0.352217
9	0.509995
10	0.509995
11	0.509995
12	0.509995
13	0.502859
14	0.502859
15	0.502859
16	0.502859

[0045] The offsets, offsetLow1(n) and offsetLow2(n) are vectors, which in one embodiment have the following values:

offsetLow1(n)=[2 2 -2 -2 2 2 -2 -2 2 2 -2 -2 2 -2 -2];

offsetLow2(n)=[1 1 -1 -1 1 1 -1 -1 1 1 -1 -1 1 1 -1];

[0046] Applying the above offset vectors to the low frequency tolerance equation results in the following expressions of the low frequency tolerance test, based upon the filter number:

TABLE 7

Filter	Criteria
1	$Klf(1) * NE(3) - NE(2) \geq C4$
2	$Klf(2) * NE(4) - NE(3) \geq C4$
3	$Klf(3) * NE(1) - NE(2) \geq C4$
4	$Klf(4) * NE(2) - NE(3) \geq C4$
5	$Klf(5) * NE(7) - NE(6) \geq C4$
6	$Klf(6) * NE(8) - NE(7) \geq C4$
7	$Klf(7) * NE(5) - NE(6) \geq C4$
8	$Klf(8) * NE(6) - NE(7) \geq C4$

9	Klf(9)*NE(11) - NE(10) ≥ C4
10	Klf(10)*NE(12) - NE(11) ≥ C4
11	Klf(11)*NE(9) - NE(10) ≥ C4
12	Klf(12)*NE(10) - NE(11) ≥ C4
13	Klf(13)*NE(15) - NE(14) ≥ C4
14	Klf(14)*NE(16) - NE(15) ≥ C4
15	Klf(15)*NE(13) - NE(14) ≥ C4
16	Klf(16)*NE(14) - NE(15) ≥ C4

[0047] The fifth criterion is a high frequency tolerance test. The high frequency tolerance test assesses whether the high frequency component of a suspected DTMF tone falls within the accepted tolerances. According to ITU recommendations, the high frequency signal must be within 1.5% of the target high frequency to qualify as a detected signal. One method of assessing the extent to which the high frequency signal meets this criteria is through assessing the extent to which that component of the signal is removed by the notch filter. A method of making that assessment is to compare the relative signal energies of other notch filters that include a notch at the high frequency.

[0048] In one embodiment, the high frequency tolerance test may be expressed as:

$$\text{Khf}(n) * \text{NE}(n + \text{offsetHigh1}(n)) - \text{NE}(n + \text{offsetHigh2}(n)) \geq$$

C5

where NE() is the signal energy, n is the filter number of the filter having a minimum signal energy, offsetHigh1(n) is an offset for filter n to select a filter having a notch at the high frequency component, offsetHigh2(n) is an offset for filter n to select another filter having a notch at the high frequency component, and Khf and C5 are empirically determined constants. In one embodiment, C5 is -0.025 and Khf(n)

has the values shown in the table below:

Table 8	
Filter No.	Khf
1	0.424951
2	0.428692
3	0.603381
4	0.596203
5	0.424951
6	0.428692
7	0.603381
8	0.596203
9	0.424951
10	0.428692
11	0.603381
12	0.596203
13	0.424951
14	0.428692
15	0.603381
16	0.596203

[0049] The offsets, $\text{offsetHigh1}(n)$ and $\text{offsetHigh2}(n)$ are vectors, which in one embodiment have the following values:

$\text{offsetHigh1}(n) = [8 \ 8 \ 8 \ 8 \ 8 \ 8 \ 8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8 \ -8];$

$\text{offsetHigh2}(n) = [4 \ 4 \ 4 \ 4 \ 4 \ 4 \ 4 \ -4 \ -4 \ -4 \ -4 \ -4 \ -4 \ -4 \ -4];$

[0050] Applying the above offset vectors to the high frequency tolerance equation results in the following expressions of the high frequency tolerance test, based upon the filter number:

TABLE 9

Filter	Criteria
1	$\text{Khf}(1) * \text{NE}(9) - \text{NE}(5) \geq C5$
2	$\text{Khf}(2) * \text{NE}(10) - \text{NE}(6) \geq C5$
3	$\text{Khf}(3) * \text{NE}(11) - \text{NE}(7) \geq C5$
4	$\text{Khf}(4) * \text{NE}(12) - \text{NE}(8) \geq C5$
5	$\text{Khf}(5) * \text{NE}(13) - \text{NE}(9) \geq C5$
6	$\text{Khf}(6) * \text{NE}(14) - \text{NE}(10) \geq C5$
7	$\text{Khf}(7) * \text{NE}(15) - \text{NE}(11) \geq C5$
8	$\text{Khf}(8) * \text{NE}(16) - \text{NE}(12) \geq C5$
9	$\text{Khf}(9) * \text{NE}(1) - \text{NE}(5) \geq C5$
10	$\text{Khf}(10) * \text{NE}(2) - \text{NE}(6) \geq C5$

11		$\text{Khf}(11) * \text{NE}(3) - \text{NE}(7) \geq C5$
12		$\text{Khf}(12) * \text{NE}(4) - \text{NE}(8) \geq C5$
13		$\text{Khf}(13) * \text{NE}(5) - \text{NE}(9) \geq C5$
14		$\text{Khf}(14) * \text{NE}(6) - \text{NE}(10) \geq C5$
15		$\text{Khf}(15) * \text{NE}(7) - \text{NE}(11) \geq C5$
16		$\text{Khf}(16) * \text{NE}(8) - \text{NE}(12) \geq C5$

[0051] The sixth criterion is an input signal energy test. The input signal energy test determines whether the signal energy of the input packetized linear voice signal 22 is greater than an empirically determined threshold value, C6. In one embodiment, the threshold value C6 is 0.001. The energy calculation in this sixth criterion an absolute frame energy calculation for the packetized linear voice signal 22, instead of the normalized calculations used in the other criteria.

[0052] The seventh criterion is a 1004 Hz test. The 1004 Hz test is intended to reject DTMF tone indications that result from the presence of a 1004 Hz signal, which has been found to trigger false DTMF detections. The signal energy of the 1004 Hz filtered signal 26 is compared to a threshold value, C7. If the signal energy of the 1004 Hz filtered signal 26 is greater than the empirically determined threshold value C7, then this criterion is met. In one embodiment, the threshold value is 0.01.

[0053] The eighth criterion is a dial tone test. The dial tone test is intended to reject DTMF tone indications that result from the presence of dial tone frequencies, which have been found to trigger false DTMF detections. The signal energy of the dial tone filtered signal 28 is compared to a threshold value, C8. If the signal energy of the dial tone filtered signal 28 is greater than the empirically determined threshold value

C8, then this criterion is met. In one embodiment, the threshold value is 1.

[0054] Referring still to Figure 2, if the threshold criteria are met in step 106, then the threshold criteria evaluation module 108 generates a DTMF indicator 32. The DTMF indicator 32 is a signal indicating that a DTMF tone is present in the packetized linear voice signal 22. The DTMF indicator 32 may further include information regarding which DTMF tone has been detected in the packetized linear voice signal 22.

[0055] Although embodiments of the present invention are described above with reference to eight specific criteria that must be met to signify a DTMF tone, it will be appreciated that fewer or more criteria may be applied, and that a DTMF tone could be indicated if a subset of the criteria are met. Variations in the criteria, the thresholds, and in the manner of adjudging the presence of a DTMF tone from the criteria results will be understood by those of ordinary skill in the art when considered in light of the above description.

[0056] The present invention may be embodied in other specific forms without departing from the spirit or essential characteristics thereof. Certain adaptations and modifications of the invention will be obvious to those skilled in the art. Therefore, the above discussed embodiments are considered to be illustrative and not restrictive, the scope of the invention being indicated by the appended claims rather than the foregoing description, and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced therein.